

# Measured Exit Plane Properties of a Low-Power Simulated-Hydrazine Arcjet

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## Introduction

IN two previous papers on the 1-kW hydrazine arcjet,<sup>1,2</sup> two types of electrostatic probe diagnostics were used at the nozzle exit plane to measure electron density  $n_e$ , electron temperature  $T_e$ , ion Mach number, plasma velocity  $u_i$ , gas temperature  $T_g$ , and related quantities. All measurements were performed at 10 A and 50 mg/s propellant mass flow on a NASA Lewis Research Center design,<sup>3</sup> at a specific power of  $P/\dot{m} = 22.4$  MJ/kg. These measurements were then compared to the two-temperature chemical nonequilibrium numerical arcjet model of Megli et al.<sup>4,5</sup> The quantities  $n_e$ ,  $T_e$ , and ion Mach number were determined with a novel quadruple electrostatic probe swept across the exit plane, with the probe axis parallel to the flow velocity.<sup>1,6</sup> The plasma velocity was measured with a double electrostatic probe using a technique similar to current modulation velocimetry (CMV).<sup>2,6</sup> Both radial and axial variations of plasma properties were measured and compared to the numerical results.

This Note presents further results for  $P/\dot{m} = 19.8$  MJ/kg and  $P/\dot{m} = 26.0$  MJ/kg (Ref. 6). The arcjet operating conditions are given in Table 1. This range of  $P/\dot{m}$  is representative of the stable operating range of this arcjet on simulated hydrazine (1 mole  $N_2$ , 2 moles  $H_2$ ). The specific impulse is interpolated from data acquired elsewhere on a comparable thruster.<sup>3</sup>

The quadruple probe combines the triple probe method of Chen and Sekiguchi,<sup>7</sup> first applied to electric thruster plumes by Tilley et al.,<sup>8,9</sup> with the crossed probe theory of Kanal,<sup>10</sup> first applied to a single-species plasma by Johnson and Murphree<sup>11</sup> and to a two-species plasma by Burton and Bufton.<sup>1</sup> The quadruple probe was first applied to an electric thruster plume by DelMedico<sup>12</sup> and Burton et al.<sup>13</sup>

The plasma velocity, assumed to equal the ion velocity  $u_i$ , is determined by a modification of a technique first developed by Pobst et al.,<sup>14</sup> in which the arc current is briefly interrupted and the resulting deficit in electron density is convected at the plasma velocity and either detected optically<sup>14</sup> or by a double time-of-flight (TOF) electrostatic probe.<sup>2</sup> Radial velocity profiles generated by this technique are accurate to  $\pm 500$  m/s and provide excellent agreement with those generated by numerical modeling.<sup>4</sup>

## Results and Discussion

The effect of varying  $P/\dot{m}$  on the anode temperature and the exit-plane quantities  $T_e$ ,  $n_e$ ,  $u_i$ , and the gas temperature  $T_g$  is shown in Table 2 and Figs. 1–3. The quadruple probe location is 2.2 mm downstream of the exit plane, and the uncertainty in the experimental  $T_e$  measurement is estimated to be  $\pm 1000$  K, due to uncertainties in the floating potential measurement and theoretical approximations.  $T_e$  decreases on the centerline by 400 K as  $P/\dot{m}$  is increased 13% at 10 A arc current and then increases by 1800 K as  $P/\dot{m}$  is increased an additional 16% and current is increased from 10 to 11 A, which

suggests that  $T_e$  is primarily a function of arc current. Previous measurements<sup>6</sup> of the radial variation of  $T_e$  show that the profile is flat, i.e., invariant with radius for a given  $P/\dot{m}$ .

The measurement of  $n_e$  as a function of radius shows little variation with  $P/\dot{m}$  (Fig. 1). The experimental error in  $n_e$  is  $\pm 50\%$  (Ref. 6), due both to the standard deviation in the measurements and a propagated uncertainty in  $T_e$ . The curves fall within  $\pm 12\%$  and are roughly Gaussian, with a peak value of  $n_e = 4 \times 10^{12}$  cm<sup>-3</sup>. This value compares to a density of  $1-2 \times 10^{13}$  cm<sup>-3</sup> found by emission spectroscopy.<sup>15</sup>

The measurement of  $u_i$  as a function of radius shows somewhat more variation with  $P/\dot{m}$  (Fig. 2). The experimental error in  $u_i$  is  $\pm 0.5$  km/s, due to uncertainties in plasma composition, probe voltage and current, and probe alignment.<sup>6</sup> The centerline velocity is 5.5, 6.6, and 8.0 km/s, increasing with  $P/\dot{m}$ , and corresponding to mean exhaust velocities based on  $I_{sp}$  of 3.9, 4.1, and 4.3 km/s. The increase in  $u_i$  of 2500 m/s over the range of operation is significantly larger than the uncertainty in the probe measurement. The bulk of the velocity variation with  $P/\dot{m}$  occurs within a 4-mm-diam core flow on axis, with little variation occurring in the viscous region near the wall.

The largest variation with  $P/\dot{m}$  occurs with the gas temperature  $T_g$  (Fig. 3). The measurement technique overpredicts  $T_g$  because the perpendicular probe is off-axis by 2 mm, reducing the current collected. A 10% undercollection decreases the sound speed by 20% and the temperature by 35%, so that the overall experimental uncertainty from the combined quadruple probe and TOF probe measurements is  $+5/-50\%$ .  $T_g$  on the centerline at  $P/\dot{m} = 19.8$  MJ/kg is predicted to be only 1200 K, only slightly higher than the anode temperature (Table 2). At  $P/\dot{m} = 22.4$  MJ/kg,  $T_g$  increases on the centerline to 3000 K, and at  $P/\dot{m} = 26.0$  MJ/kg,  $T_g = 7000$  K. The profiles are roughly Gaussian.

These results are in approximate agreement with previous results by Zube and Myers<sup>16</sup> of spectroscopically determined temperatures within the nozzle of a similar arcjet, operated at 9 A (21.0 MJ/kg) and

Table 1 Operating range of 1 kW hydrazine arcjet

| Power, W | Current, A | Mass flow rate, mg/s | $P/\dot{m}$ , MJ/kg | Specific impulse, s |
|----------|------------|----------------------|---------------------|---------------------|
| 1188     | 10         | 60                   | 19.8                | 397                 |
| 1120     | 10         | 50                   | 22.4                | 414                 |
| 1170     | 11         | 45                   | 26.0                | 440                 |

Table 2 Operating temperatures of 1 kW  $N_2/H_2$  arcjet

| $P/\dot{m}$ , MJ/kg | Arc current, A | Anode temp, K | Centerline $T_e$ , K |
|---------------------|----------------|---------------|----------------------|
| 19.8                | 10             | 1160          | 7300                 |
| 22.4                | 10             | 1220          | 6900                 |
| 26.0                | 11             | 1320          | 8700                 |

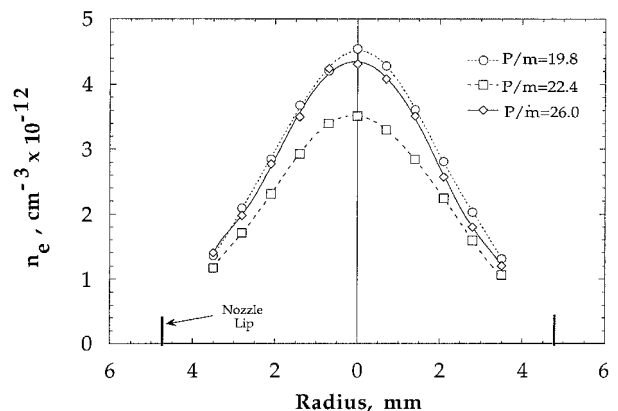


Fig. 1 Radial  $n_e$  profiles measured by quadruple probe for the three thruster operating conditions examined; uncertainty in  $n_e$  is  $\pm 50\%$  and is not shown.

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Table 3 Comparison of centerline ( $x = 2.2$  mm)  $n_e$  and  $T_e$  measurements of this study with the numerical exit-plane predictions of Megli et al.<sup>4</sup>

| Case | Experiment          |                          |           |              | Numerical model |                          |           |              |
|------|---------------------|--------------------------|-----------|--------------|-----------------|--------------------------|-----------|--------------|
|      | $P/\dot{m}$ , MJ/kg | $n_e$ , cm <sup>-3</sup> | $T_e$ , K | $u_i$ , km/s | $T_g$           | $n_e$ , cm <sup>-3</sup> | $T_e$ , K | $u_i$ , km/s |
| 1    | 19.8                | $4.6 \times 10^{12}$     | 7300      | 5.5          | 1200            | $3.5 \times 10^{14}$     | 3250      | 6.9          |
| 2    | 22.4                | $3.5 \times 10^{12}$     | 7000      | 6.5          | 3000            | $3.1 \times 10^{14}$     | 3030      | 6.7          |
| 3    | 26.0                | $4.3 \times 10^{12}$     | 8700      | 8.0          | 7000            | $3.2 \times 10^{14}$     | 3160      | 6.8          |

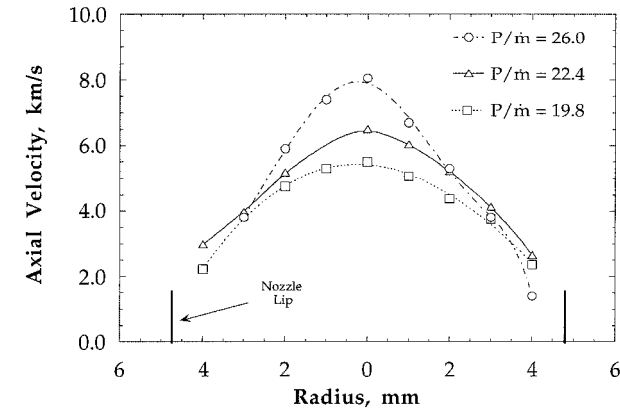


Fig. 2 Radial profiles of the plasma axial velocity  $u_i$  measured by quadrupole probe for three different thruster specific powers  $P/\dot{m}$ ; error bars are not shown, but are typically  $\pm 0.5$  km/s.

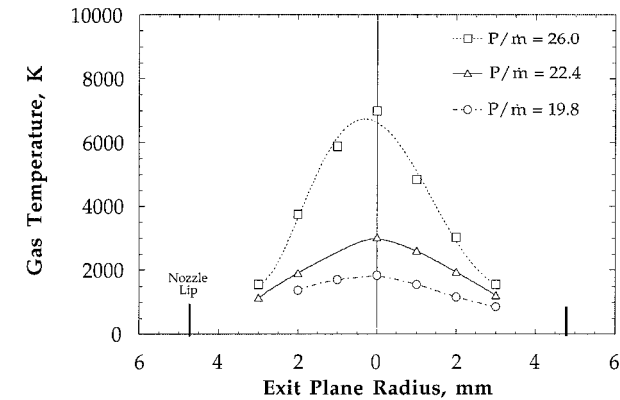


Fig. 3 Estimated gas temperature profiles based on measurements of  $u_i$  and  $u_i/c_{m,H^+}$  by quadrupole probe for three values of thruster specific power; uncertainty in  $T_g$  estimates is  $\pm 5\text{--}50\%$ .

12 A (28.0 MJ/kg). They found, at a location 3.3 mm upstream of the exit plane, a nitrogen atom excitation temperature of 8400 K (9 A) and 10,000 K (12 A). The nitrogen molecule vibrational temperature was 2300 K at both currents, and nitrogen molecule rotational temperatures were 2000 K (9 A) and 2600 K (12 A), with the latter to within  $\pm 12.5\%$ . The corresponding measurements of  $T_e$  and  $T_g$  observed here for 10 A and  $P/\dot{m} = 22.4$  MJ/kg are  $T_e \sim 7000$  K and  $T_g \sim 2500$  K. Zube and Myers<sup>16</sup> did not observe the 7000 K  $\pm 5\text{--}50\%$  temperature on centerline indicated here for  $P/\dot{m} = 26$  MJ/kg, suggesting that the probe considerably result overstates  $T_g$  at this condition.

A comparison of these measurements with numerical model predictions<sup>4</sup> of  $n_e$  and  $T_e$  is shown in Table 3, for similar  $I$  and  $\dot{m}$ . The experiments were conducted with the probe centered at an axial location of  $x = 2.2$  mm, and the model predictions represent centerline exit plane results. Although the electron densities differ by  $\sim 2$  orders of magnitude due to the large axial gradient near the exit plane<sup>15</sup> and electrostatic probe measurements made 40–100 mm downstream.<sup>17</sup> The trends in  $n_e$  are very similar for the model and experiments. Similarly, the trends in the electron temperature mea-

surements and model predictions are the same, despite the different magnitudes in  $T_e$ .

The model axial velocity predictions, despite the fact that the model predicts increased  $I_{sp}$  with increased  $P/\dot{m}$  similar to the measured results,<sup>4</sup> vary less than  $\sim 2\%$  for the range of specific power investigated in this study (Table 3). This could be an indication that the density profiles in the arcjet plume and those predicted by the model may be vastly different, a distinction we were unable to detect.

Table 3 also shows centerline values of the predicted gas temperature  $T_g$  at the exit plane vs the  $T_g$  measurement. The apparent large increase in the experimental values of  $T_g$  with increases in  $P/\dot{m}$  may imply a corresponding decrease in the centerline bulk gas density, a trend consistent with the earlier argument that the plasma density profiles of the model and experiment may be quite different despite the accurate model prediction of  $I_{sp}$ .

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